

Crossville, Inc.
P1 Facility, Source No. 18-0086
Crossville, TN

Source No. 18-0086-03, Kilns 1 & 2, Uncontrolled Maximum Potential Emissions

The maximum process material input rate is 4,350 pounds per hour for each kiln. This results in a total maximum input of 8,700 pounds per hour for this source.

Hourly and yearly maximum potential emissions of the following pollutants are estimated based on a February 12, 2009 stack test performed on Kiln 1 at Crossville Plant 1. Emissions are scaled to the kiln's maximum tile throughput rates.

$$\begin{aligned}\text{PM: } & (0.173 \text{ lb}_{\text{pm}} / \text{hr}) * (4350 \text{ lb}_{\text{tile max}} / \text{hr} \div 4329 \text{ lb}_{\text{tested}} / \text{hr}) * 2 \text{ kilns} = \mathbf{0.348 \text{ lb}_{\text{pm}} / \text{hr}} \\ & (0.3477 \text{ lb}_{\text{pm}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{1.52 \text{ tons}_{\text{pm}} / \text{yr}}\end{aligned}$$

$$\begin{aligned}\text{SO}_2: & (1.31 \text{ lb}_{\text{SO}_2} / \text{hr}) * (4350 \text{ lb}_{\text{tile max}} / \text{hr} \div 4329 \text{ lb}_{\text{tested}} / \text{hr}) * 2 \text{ kilns} = \mathbf{2.63 \text{ lb}_{\text{SO}_2} / \text{hr}} \\ & (2.633 \text{ lb}_{\text{SO}_2} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{11.5 \text{ tons}_{\text{SO}_2} / \text{yr}}\end{aligned}$$

$$\begin{aligned}\text{NO}_X: & (1.21 \text{ lb}_{\text{NO}_X} / \text{hr}) * (4350 \text{ lb}_{\text{tile max}} / \text{hr} \div 4329 \text{ lb}_{\text{tested}} / \text{hr}) * 2 \text{ kilns} = \mathbf{2.43 \text{ lb}_{\text{NO}_X} / \text{hr}} \\ & (2.432 \text{ lb}_{\text{NO}_X} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{10.7 \text{ tons}_{\text{NO}_X} / \text{yr}}\end{aligned}$$

$$\begin{aligned}\text{CO: } & (2.62 \text{ lb}_{\text{CO}} / \text{hr}) * (4350 \text{ lb}_{\text{tile max}} / \text{hr} \div 4329 \text{ lb}_{\text{tested}} / \text{hr}) * 2 \text{ kilns} = \mathbf{5.27 \text{ lb}_{\text{CO}} / \text{hr}} \\ & (5.265 \text{ lb}_{\text{CO}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{23.1 \text{ tons}_{\text{CO}} / \text{yr}}\end{aligned}$$

$$\begin{aligned}\text{HCl: } & (0.068 \text{ lb}_{\text{HCl}} / \text{hr}) * (4350 \text{ lb}_{\text{tile max}} / \text{hr} \div 4329 \text{ lb}_{\text{tested}} / \text{hr}) * 2 \text{ kilns} = \mathbf{0.137 \text{ lb}_{\text{HCl}} / \text{hr}} \\ & (0.1367 \text{ lb}_{\text{HCl}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.599 \text{ tons}_{\text{HCl}} / \text{yr}}\end{aligned}$$

$$\begin{aligned}\text{HF: } & (0.20 \text{ lb}_{\text{HF}} / \text{hr}) * (4350 \text{ lb}_{\text{tile max}} / \text{hr} \div 4329 \text{ lb}_{\text{tested}} / \text{hr}) * 2 \text{ kilns} = \mathbf{0.40 \text{ lb}_{\text{HF}} / \text{hr}} \\ & (0.402 \text{ lb}_{\text{HF}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{1.8 \text{ tons}_{\text{HF}} / \text{yr}}\end{aligned}$$

VOC emissions are based on AP-42 section 11.7, Ceramic Products Manufacturing.

$$\begin{aligned}\text{VOC: } & (0.43 \text{ lb}_{\text{VOC}} / \text{ton}) * (4350 \text{ lb}_{\text{tile max}} / \text{hr}) * (1 \text{ ton} / 2000 \text{ lb}) * 2 \text{ kilns} = \mathbf{1.9 \text{ lb}_{\text{VOC}} / \text{hr}} \\ & (1.87 \text{ lb}_{\text{VOC}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{8.2 \text{ tons}_{\text{VOC}} / \text{yr}}\end{aligned}$$

Source No. 18-0086-04, Spray Dryer #1, Uncontrolled Maximum Potential Emissions

The maximum clay slurry solids throughput rate for Spray Dryer #1 is 17,807 pounds per hour.

Emissions for particulate matter are conservatively estimated based on the permitted maximum rate. This rate is based on an April 1, 2009 stack test performed on Spray Dryer #1 with a 30% safety factor

included. The spray dryer has a wet scrubber installed with attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for the spray dryer are calculated post scrubber.

PM: **2.74 lb_{PM} / hr**

$$(2.74 \text{ lb}_{\text{PM}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{12.0 \text{ tons}_{\text{PM}} / \text{yr}}$$

Emissions for the following pollutants are estimated using AP-42 factors for natural gas combustion section 1.4.

Btu input = 7,788,000 Btu/hr

Fuel Usage: $(7,788,000 \text{ Btu} / \text{hr}) * (1 \text{ ft}^3 \text{ natural gas} / 1,020 \text{ Btu}) = \mathbf{7,635 \text{ ft}^3 / \text{hr}}$

SO₂ $(0.6 \text{ lb} / 1,000,000 \text{ ft}^3) * (7,635 \text{ ft}^3 / \text{hr}) = \mathbf{0.0 \text{ lb} / \text{hr}}$
 $(0.00 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.0 \text{ ton} / \text{yr}}$

CO: $(84 \text{ lbs} / 1,000,000 \text{ ft}^3) * (7,635 \text{ ft}^3 / \text{hr}) = \mathbf{0.64 \text{ lb} / \text{hr}}$
 $(0.641 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{2.8 \text{ tons} / \text{yr}}$

VOC: $(5.5 \text{ lbs} / 1,000,000 \text{ ft}^3) * (7,635 \text{ ft}^3 / \text{hr}) = \mathbf{0.04 \text{ lb} / \text{hr}}$
 $(0.042 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.18 \text{ ton} / \text{yr}}$

NO_x: $(100 \text{ lbs} / 1,000,000 \text{ ft}^3) * (7,635 \text{ ft}^3 / \text{hr}) = \mathbf{0.764 \text{ lb} / \text{hr}}$
 $(0.7635 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{3.34 \text{ tons} / \text{yr}}$

Source No. 18-0086-05, Natural Gas-Fired Heater, Uncontrolled Maximum Potential Emissions

Emissions for the following pollutants are estimated using AP-42 factors for natural gas combustion section 1.4.

Btu input = 2,190,000 Btu/hr

Fuel Usage: $(2,190,000 \text{ Btu} / \text{hr}) * (1 \text{ ft}^3 \text{ natural gas} / 1,020 \text{ Btu}) = \mathbf{2,147 \text{ ft}^3 / \text{hr}}$

PM: $(7.6 \text{ lb} / 1,000,000 \text{ ft}^3) * (2,147 \text{ ft}^3 / \text{hr}) = \mathbf{0.02 \text{ lb} / \text{hr}}$

$$(0.016 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{0.07 \text{ ton / yr}}$$

$$\begin{aligned} \text{SO}_2: \quad & (0.6 \text{ lb / 1,000,000 ft}^3) * (2,147 \text{ ft}^3 / \text{hr}) = \mathbf{0.0 \text{ lb / hr}} \\ & (0.00 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{0.0 \text{ ton / yr}} \end{aligned}$$

$$\begin{aligned} \text{CO:} \quad & (84 \text{ lbs / 1,000,000 ft}^3) * (2,147 \text{ ft}^3 / \text{hr}) = \mathbf{0.18 \text{ lb / hr}} \\ & (0.180 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{0.79 \text{ tons / yr}} \end{aligned}$$

$$\begin{aligned} \text{VOC:} \quad & (5.5 \text{ lbs / 1,000,000 ft}^3) * (2,147 \text{ ft}^3 / \text{hr}) = \mathbf{0.01 \text{ lb / hr}} \\ & (0.012 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{0.05 \text{ ton / yr}} \end{aligned}$$

$$\begin{aligned} \text{NO}_x: \quad & (100 \text{ lbs / 1,000,000 ft}^3) * (2,147 \text{ ft}^3 / \text{hr}) = \mathbf{0.215 \text{ lb / hr}} \\ & (0.2147 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{0.940 \text{ tons / yr}} \end{aligned}$$

Source No. 18-0086-11, Dust Collection System with Baghouse for Transfer Points from Conveyor to Conveyor and Drop Points into Press Silo, Uncontrolled Maximum Potential Emissions

Emissions for particulate matter are conservatively estimated based on the permitted maximum rate. This dust collection system has attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for this source are calculated post baghouse.

$$\begin{aligned} \text{PM:} \quad & \mathbf{3.6 \text{ lb}_{PM} / \text{hr}} \\ & (3.6 \text{ lb}_{PM} / \text{hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{15.8 \text{ tons}_{PM} / \text{yr}} \end{aligned}$$

Source No. 18-0086-12, Spray Dryer #2, Uncontrolled Maximum Potential Emissions

The maximum clay slurry solids throughput rate for Spray Dryer #1 is 18,000 pounds per hour.

Emissions for particulate matter are conservatively estimated based on the permitted maximum rate. This rate is based on Federal New Source Performance Standards Subpart UUU. The spray dryer has a wet scrubber installed with attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for the spray dryer are calculated post scrubber.

$$\begin{aligned} \text{PM:} \quad & \mathbf{1.88 \text{ lb}_{pm} / \text{hr}} \\ & (1.88 \text{ lb}_{pm} / \text{hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{8.23 \text{ tons}_{pm} / \text{yr}} \end{aligned}$$

Emissions for the following pollutants are estimated using AP-42 factors for natural gas combustion section 1.4.

Fuel Usage: **7,788 ft³ / hr**

SO₂ (0.6 lb / 1,000,000 ft³) * (7,788 ft³ / hr) = **0.0 lb / hr**
(0.00 lb / hr) * (8760 hrs / yr) * (1 ton / 2000 lbs) = **0.0 ton / yr**

CO: (84 lbs / 1,000,000 ft³) * (7,788 ft³ / hr) = **0.65 lb / hr**
(0.654 lb / hr) * (8760 hrs / yr) * (1 ton / 2000 lbs) = **2.9 tons / yr**

VOC: (5.5 lbs / 1,000,000 ft³) * (7,788 ft³ / hr) = **0.04 lb / hr**
(0.043 lb / hr) * (8760 hrs / yr) * (1 ton / 2000 lbs) = **0.19 ton / yr**

NO_x: (100 lbs / 1,000,000 ft³) * (7,788 ft³ / hr) = **0.779 lb / hr**
(0.7788 lb / hr) * (8760 hrs / yr) * (1 ton / 2000 lbs) = **3.41 tons / yr**

Source No. 18-0086-13, Kiln 4, Uncontrolled Maximum Potential Emissions

The maximum process material input rate is 8,200 pounds per hour for this source.

Hourly and yearly maximum potential emissions of the following pollutants are estimated based on an April 1, 2009 stack test performed on Kiln 4 at Crossville Plant 1. Emissions are scaled to the kiln's maximum tile throughput rates.

PM: (0.268 lb_{pm} / hr) * (8200 lb_{tile max} / hr ÷ 8161 lb_{tested} / hr) = **0.269 lb_{pm} / hr**
(0.2693 lb_{pm} / hr) * (8760 hrs / yr) * (1 ton / 2000 lbs) = **1.18 tons_{pm} / yr**

SO₂: (2.28 lb_{SO2} / hr) * (8200 lb_{tile max} / hr ÷ 8161 lb_{tested} / hr) = **2.29 lb_{SO2} / hr**
(2.291 lb_{SO2} / hr) * (8760 hrs / yr) * (1 ton / 2000 lbs) = **10.0 tons_{SO2} / yr**

NO_x: (1.43 lb_{NOX} / hr) * (8200 lb_{tile max} / hr ÷ 8161 lb_{tested} / hr) = **1.44 lb_{NOX} / hr**
(1.437 lb_{NOX} / hr) * (8760 hrs / yr) * (1 ton / 2000 lbs) = **6.29 tons_{NOX} / yr**

CO: (3.89 lb_{CO} / hr) * (8200 lb_{tile max} / hr ÷ 8161 lb_{tested} / hr) = **3.91 lb_{CO} / hr**
(3.909 lb_{CO} / hr) * (8760 hrs / yr) * (1 ton / 2000 lbs) = **17.1 tons_{CO} / yr**

HCl: (0.200 lb_{HCl} / hr) * (8200 lb_{tile max} / hr ÷ 8161 lb_{tested} / hr) = **0.201 lb_{HCl} / hr**
(0.2010 lb_{HCl} / hr) * (8760 hrs / yr) * (1 ton / 2000 lbs) = **0.880 tons_{HCl} / yr**

HF: (0.440 lb_{HF} / hr) * (8200 lb_{tile max} / hr ÷ 8161 lb_{tested} / hr) = **0.442 lb_{HF} / hr**

$$(0.4421 \text{ lb}_{\text{HF}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{1.94 \text{ tons}_{\text{HF}} / \text{yr}}$$

VOC emissions are based on AP-42 section 11.7, Ceramic Products Manufacturing.

$$\text{VOC: } (0.43 \text{ lb}_{\text{VOC}} / \text{ton}) * (8200 \text{ lb}_{\text{tile max}} / \text{hr}) * (1 \text{ ton} / 2000 \text{ lb}) = \mathbf{1.8 \text{ lb}_{\text{VOC}} / \text{hr}}$$

$$(1.76 \text{ lb}_{\text{VOC}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{7.7 \text{ tons}_{\text{VOC}} / \text{yr}}$$

Source No. 18-0086-14, Natural Gas-Fired Tunnel Dryer No. 1, Uncontrolled Maximum Potential Emissions

Emissions for the following pollutants are estimated using AP-42 factors for natural gas combustion section 1.4.

Btu input = 6,100,000 Btu/hr

$$\text{Fuel Usage: } (6,100,000 \text{ Btu} / \text{hr}) * (1 \text{ ft}^3 \text{ natural gas} / 1,020 \text{ Btu}) = \mathbf{5,980 \text{ ft}^3 / \text{hr}}$$

$$\text{PM: } (7.6 \text{ lbs} / 1,000,000 \text{ ft}^3) * (5,980 \text{ ft}^3 / \text{hr}) = \mathbf{0.05 \text{ lb} / \text{hr}}$$

$$(0.045 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.20 \text{ ton} / \text{yr}}$$

$$\text{SO}_2: (0.6 \text{ lb} / 1,000,000 \text{ ft}^3) * (5,980 \text{ ft}^3 / \text{hr}) = \mathbf{0.0 \text{ lb} / \text{hr}}$$

$$(0.00 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.0 \text{ ton} / \text{yr}}$$

$$\text{CO: } (84 \text{ lbs} / 1,000,000 \text{ ft}^3) * (5,980 \text{ ft}^3 / \text{hr}) = \mathbf{0.50 \text{ lb} / \text{hr}}$$

$$(0.502 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{2.2 \text{ tons} / \text{yr}}$$

$$\text{VOC: } (5.5 \text{ lbs} / 1,000,000 \text{ ft}^3) * (5,980 \text{ ft}^3 / \text{hr}) = \mathbf{0.03 \text{ lb} / \text{hr}}$$

$$(0.033 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.14 \text{ ton} / \text{yr}}$$

$$\text{NO}_x: (100 \text{ lbs} / 1,000,000 \text{ ft}^3) * (5,980 \text{ ft}^3 / \text{hr}) = \mathbf{0.598 \text{ lb} / \text{hr}}$$

$$(0.5980 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{2.62 \text{ tons} / \text{yr}}$$

Source No. 18-0086-15, Natural Gas-Fired Tunnel Dryer No. 2, Uncontrolled Maximum Potential Emissions

Emissions for the following pollutants are estimated using AP-42 factors for natural gas combustion section 1.4.

Btu input = 6,100,000 Btu/hr

Fuel Usage: $(6,100,000 \text{ Btu / hr}) * (1 \text{ ft}^3 \text{ natural gas / } 1,020 \text{ Btu}) = \mathbf{5,980 \text{ ft}^3 / \text{hr}}$

PM: $(7.6 \text{ lbs / } 1,000,000 \text{ ft}^3) * (5,980 \text{ ft}^3 / \text{hr}) = \mathbf{0.05 \text{ lb / hr}}$
 $(0.045 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / } 2000 \text{ lbs}) = \mathbf{0.20 \text{ ton / yr}}$

SO₂: $(0.6 \text{ lb / } 1,000,000 \text{ ft}^3) * (5,980 \text{ ft}^3 / \text{hr}) = \mathbf{0.0 \text{ lb / hr}}$
 $(0.00 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / } 2000 \text{ lbs}) = \mathbf{0.0 \text{ ton / yr}}$

CO: $(84 \text{ lbs / } 1,000,000 \text{ ft}^3) * (5,980 \text{ ft}^3 / \text{hr}) = \mathbf{0.50 \text{ lb / hr}}$
 $(0.502 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / } 2000 \text{ lbs}) = \mathbf{2.2 \text{ tons / yr}}$

VOC: $(5.5 \text{ lbs / } 1,000,000 \text{ ft}^3) * (5,980 \text{ ft}^3 / \text{hr}) = \mathbf{0.03 \text{ lb / hr}}$
 $(0.033 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / } 2000 \text{ lbs}) = \mathbf{0.14 \text{ ton / yr}}$

NO_x: $(100 \text{ lbs / } 1,000,000 \text{ ft}^3) * (5,980 \text{ ft}^3 / \text{hr}) = \mathbf{0.598 \text{ lb / hr}}$
 $(0.5980 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / } 2000 \text{ lbs}) = \mathbf{2.62 \text{ tons / yr}}$

Source No. 18-0086-16, Vertical talc silo with fabric filter bin vent, Uncontrolled Maximum Potential Emissions

Emissions for particulate matter are conservatively estimated based on the permitted maximum rate. This dust collection system has attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for this source are calculated post baghouse.

PM: $\mathbf{1.5 \text{ lb}_{PM} / \text{hr}}$
 $(1.5 \text{ lb}_{PM} / \text{hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / } 2000 \text{ lbs}) = \mathbf{6.6 \text{ tons}_{PM} / \text{yr}}$

Source No. 18-0086-17, Natural Gas-Fired Dryer for Press #5, Uncontrolled Maximum Potential Emissions

Emissions for the following pollutants are estimated using AP-42 factors for natural gas combustion section 1.4.

Btu input = 3,930,000 Btu/hr

Fuel Usage: $(3,930,000 \text{ Btu / hr}) * (1 \text{ ft}^3 \text{ natural gas / } 1,020 \text{ Btu}) = \mathbf{3,853 \text{ ft}^3 / \text{hr}}$

PM: $(7.6 \text{ lbs / } 1,000,000 \text{ ft}^3) * (3,853 \text{ ft}^3 / \text{hr}) = \mathbf{0.03 \text{ lb / hr}}$
 $(0.029 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / } 2000 \text{ lbs}) = \mathbf{0.13 \text{ ton / yr}}$

SO₂: $(0.6 \text{ lb / } 1,000,000 \text{ ft}^3) * (3,853 \text{ ft}^3 / \text{hr}) = \mathbf{0.0 \text{ lb / hr}}$
 $(0.00 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / } 2000 \text{ lbs}) = \mathbf{0.0 \text{ ton / yr}}$

CO: $(84 \text{ lbs / } 1,000,000 \text{ ft}^3) * (3,853 \text{ ft}^3 / \text{hr}) = \mathbf{0.32 \text{ lb / hr}}$
 $(0.324 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / } 2000 \text{ lbs}) = \mathbf{1.4 \text{ tons / yr}}$

VOC: $(5.5 \text{ lbs / } 1,000,000 \text{ ft}^3) * (3,853 \text{ ft}^3 / \text{hr}) = \mathbf{0.02 \text{ lb / hr}}$
 $(0.021 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / } 2000 \text{ lbs}) = \mathbf{0.09 \text{ ton / yr}}$

NO_x: $(100 \text{ lbs / } 1,000,000 \text{ ft}^3) * (3,853 \text{ ft}^3 / \text{hr}) = \mathbf{0.385 \text{ lb / hr}}$
 $(0.3853 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / } 2000 \text{ lbs}) = \mathbf{1.69 \text{ tons / yr}}$

Source No. 18-0086-18, Natural Gas-Fired Dryer, Uncontrolled Maximum Potential Emissions

Emissions for the following pollutants are estimated using AP-42 factors for natural gas combustion section 1.4.

Btu input = 3,930,000 Btu/hr

Fuel Usage: $(3,930,000 \text{ Btu / hr}) * (1 \text{ ft}^3 \text{ natural gas / } 1,020 \text{ Btu}) = \mathbf{3,853 \text{ ft}^3 / \text{hr}}$

PM: $(7.6 \text{ lbs / } 1,000,000 \text{ ft}^3) * (3,853 \text{ ft}^3 / \text{hr}) = \mathbf{0.03 \text{ lb / hr}}$
 $(0.029 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / } 2000 \text{ lbs}) = \mathbf{0.13 \text{ ton / yr}}$

SO₂: $(0.6 \text{ lb / } 1,000,000 \text{ ft}^3) * (3,853 \text{ ft}^3 / \text{hr}) = \mathbf{0.0 \text{ lb / hr}}$
 $(0.00 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / } 2000 \text{ lbs}) = \mathbf{0.0 \text{ ton / yr}}$

CO: $(84 \text{ lbs} / 1,000,000 \text{ ft}^3) * (3,853 \text{ ft}^3 / \text{hr}) = \mathbf{0.32 \text{ lb} / \text{hr}}$
 $(0.324 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{1.4 \text{ tons} / \text{yr}}$

VOC: $(5.5 \text{ lbs} / 1,000,000 \text{ ft}^3) * (3,853 \text{ ft}^3 / \text{hr}) = \mathbf{0.02 \text{ lb} / \text{hr}}$
 $(0.021 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.09 \text{ ton} / \text{yr}}$

NO_x: $(100 \text{ lbs} / 1,000,000 \text{ ft}^3) * (3,853 \text{ ft}^3 / \text{hr}) = \mathbf{0.385 \text{ lb} / \text{hr}}$
 $(0.3853 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{1.69 \text{ tons} / \text{yr}}$

Source No. 18-0086-19, Natural Gas-Fired Dryer, Uncontrolled Maximum Potential Emissions

Emissions for the following pollutants are estimated using AP-42 factors for natural gas combustion section 1.4.

Btu input = 3,930,000 Btu/hr

Fuel Usage: $(3,930,000 \text{ Btu} / \text{hr}) * (1 \text{ ft}^3 \text{ natural gas} / 1,020 \text{ Btu}) = \mathbf{3,853 \text{ ft}^3 / \text{hr}}$

PM: $(7.6 \text{ lbs} / 1,000,000 \text{ ft}^3) * (3,853 \text{ ft}^3 / \text{hr}) = \mathbf{0.03 \text{ lb} / \text{hr}}$
 $(0.029 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.13 \text{ ton} / \text{yr}}$

SO₂: $(0.6 \text{ lb} / 1,000,000 \text{ ft}^3) * (3,853 \text{ ft}^3 / \text{hr}) = \mathbf{0.0 \text{ lb} / \text{hr}}$
 $(0.00 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.0 \text{ ton} / \text{yr}}$

CO: $(84 \text{ lbs} / 1,000,000 \text{ ft}^3) * (3,853 \text{ ft}^3 / \text{hr}) = \mathbf{0.32 \text{ lb} / \text{hr}}$
 $(0.324 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{1.4 \text{ tons} / \text{yr}}$

VOC: $(5.5 \text{ lbs} / 1,000,000 \text{ ft}^3) * (3,853 \text{ ft}^3 / \text{hr}) = \mathbf{0.02 \text{ lb} / \text{hr}}$
 $(0.021 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.09 \text{ ton} / \text{yr}}$

NO_x: $(100 \text{ lbs} / 1,000,000 \text{ ft}^3) * (3,853 \text{ ft}^3 / \text{hr}) = \mathbf{0.385 \text{ lb} / \text{hr}}$
 $(0.3853 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{1.69 \text{ tons} / \text{yr}}$

Source No. 18-0086-23, Mori Kiln, Uncontrolled Maximum Potential Emissions

The maximum process material input rate is 850 pounds per hour.

Hourly and yearly maximum potential emissions of the following pollutants are estimated based on a February 12, 2009 stack test performed on Kiln 1 at Crossville Plant 1. Emissions are scaled to the kiln's maximum tile input rate.

$$\begin{aligned}\text{PM: } & (0.173 \text{ lb}_{\text{pm}} / \text{hr}) * (850 \text{ lb}_{\text{tile max}} / \text{hr} \div 4329 \text{ lb}_{\text{tested}} / \text{hr}) = \mathbf{0.034 \text{ lb}_{\text{pm}} / \text{hr}} \\ & (0.0340 \text{ lb}_{\text{pm}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.149 \text{ tons}_{\text{pm}} / \text{yr}}\end{aligned}$$

$$\begin{aligned}\text{SO}_2: & (1.31 \text{ lb}_{\text{SO}_2} / \text{hr}) * (850 \text{ lb}_{\text{tile max}} / \text{hr} \div 4329 \text{ lb}_{\text{tested}} / \text{hr}) = \mathbf{0.257 \text{ lb}_{\text{SO}_2} / \text{hr}} \\ & (0.2572 \text{ lb}_{\text{SO}_2} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{1.13 \text{ tons}_{\text{SO}_2} / \text{yr}}\end{aligned}$$

$$\begin{aligned}\text{NO}_x: & (1.21 \text{ lb}_{\text{NO}_x} / \text{hr}) * (850 \text{ lb}_{\text{tile max}} / \text{hr} \div 4329 \text{ lb}_{\text{tested}} / \text{hr}) = \mathbf{0.238 \text{ lb}_{\text{NO}_x} / \text{hr}} \\ & (0.2376 \text{ lb}_{\text{NO}_x} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{1.04 \text{ tons}_{\text{NO}_x} / \text{yr}}\end{aligned}$$

$$\begin{aligned}\text{CO: } & (2.62 \text{ lb}_{\text{CO}} / \text{hr}) * (850 \text{ lb}_{\text{tile max}} / \text{hr} \div 4329 \text{ lb}_{\text{tested}} / \text{hr}) = \mathbf{0.514 \text{ lb}_{\text{CO}} / \text{hr}} \\ & (0.5144 \text{ lb}_{\text{CO}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{2.25 \text{ tons}_{\text{CO}} / \text{yr}}\end{aligned}$$

$$\begin{aligned}\text{HCl: } & (0.068 \text{ lb}_{\text{HCl}} / \text{hr}) * (850 \text{ lb}_{\text{tile max}} / \text{hr} \div 4329 \text{ lb}_{\text{tested}} / \text{hr}) = \mathbf{0.013 \text{ lb}_{\text{HCl}} / \text{hr}} \\ & (0.0134 \text{ lb}_{\text{HCl}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.058 \text{ tons}_{\text{HCl}} / \text{yr}}\end{aligned}$$

$$\begin{aligned}\text{HF: } & (0.20 \text{ lb}_{\text{HF}} / \text{hr}) * (850 \text{ lb}_{\text{tile max}} / \text{hr} \div 4329 \text{ lb}_{\text{tested}} / \text{hr}) = \mathbf{0.04 \text{ lb}_{\text{HF}} / \text{hr}} \\ & (0.039 \text{ lb}_{\text{HF}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.17 \text{ tons}_{\text{HF}} / \text{yr}}\end{aligned}$$

VOC emissions are based on AP-42 section 11.7, Ceramic Products Manufacturing.

$$\begin{aligned}\text{VOC: } & (0.43 \text{ lb}_{\text{VOC}} / \text{ton}) * (850 \text{ lb}_{\text{tile max}} / \text{hr}) * (1 \text{ ton} / 2000 \text{ lb}) = \mathbf{0.18 \text{ lb}_{\text{VOC}} / \text{hr}} \\ & (0.183 \text{ lb}_{\text{VOC}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.80 \text{ tons}_{\text{VOC}} / \text{yr}}\end{aligned}$$

Source No. 18-0086-24, Mosaics Siti Kiln, Uncontrolled Maximum Potential Emissions

The maximum process material input rate is 2,500 pounds per hour.

Hourly and yearly maximum potential emissions of the following pollutants are estimated based on a February 12, 2009 stack test performed on Kiln 1 at Crossville Plant 1. Emissions are scaled to the kiln's maximum tile input rate.

$$\begin{aligned}\text{PM: } & (0.173 \text{ lb}_{\text{pm}} / \text{hr}) * (2500 \text{ lb}_{\text{tile max}} / \text{hr} \div 4329 \text{ lb}_{\text{tested}} / \text{hr}) = \mathbf{0.100 \text{ lb}_{\text{pm}} / \text{hr}} \\ & (0.1000 \text{ lb}_{\text{pm}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.438 \text{ tons}_{\text{pm}} / \text{yr}}\end{aligned}$$

$$\text{SO}_2: (1.31 \text{ lb}_{\text{SO}_2} / \text{hr}) * (2500 \text{ lb}_{\text{tile max}} / \text{hr} \div 4329 \text{ lb}_{\text{tested}} / \text{hr}) = \mathbf{0.757 \text{ lb}_{\text{SO}_2} / \text{hr}}$$

$$(0.7565 \text{ lb}_{\text{SO}_2} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{3.31 \text{ tons}_{\text{SO}_2} / \text{yr}}$$

$$\begin{aligned} \text{NO}_x: & (1.21 \text{ lb}_{\text{NO}_x} / \text{hr}) * (2500 \text{ lb}_{\text{tile max}} / \text{hr} \div 4329 \text{ lb}_{\text{tested}} / \text{hr}) = \mathbf{0.699 \text{ lb}_{\text{NO}_x} / \text{hr}} \\ & (0.6988 \text{ lb}_{\text{NO}_x} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{3.06 \text{ tons}_{\text{NO}_x} / \text{yr}} \end{aligned}$$

$$\begin{aligned} \text{CO:} & (2.62 \text{ lb}_{\text{CO}} / \text{hr}) * (2500 \text{ lb}_{\text{tile max}} / \text{hr} \div 4329 \text{ lb}_{\text{tested}} / \text{hr}) = \mathbf{1.51 \text{ lb}_{\text{CO}} / \text{hr}} \\ & (1.513 \text{ lb}_{\text{CO}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{6.63 \text{ tons}_{\text{CO}} / \text{yr}} \end{aligned}$$

$$\begin{aligned} \text{HCl:} & (0.068 \text{ lb}_{\text{HCl}} / \text{hr}) * (2500 \text{ lb}_{\text{tile max}} / \text{hr} \div 4329 \text{ lb}_{\text{tested}} / \text{hr}) = \mathbf{0.039 \text{ lb}_{\text{HCl}} / \text{hr}} \\ & (0.0393 \text{ lb}_{\text{HCl}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.172 \text{ tons}_{\text{HCl}} / \text{yr}} \end{aligned}$$

$$\begin{aligned} \text{HF:} & (0.20 \text{ lb}_{\text{HF}} / \text{hr}) * (2500 \text{ lb}_{\text{tile max}} / \text{hr} \div 4329 \text{ lb}_{\text{tested}} / \text{hr}) = \mathbf{0.12 \text{ lb}_{\text{HF}} / \text{hr}} \\ & (0.116 \text{ lb}_{\text{HF}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.51 \text{ tons}_{\text{HF}} / \text{yr}} \end{aligned}$$

VOC emissions are based on AP-42 section 11.7, Ceramic Products Manufacturing.

$$\begin{aligned} \text{VOC:} & (0.43 \text{ lb}_{\text{VOC}} / \text{ton}) * (2500 \text{ lb}_{\text{tile max}} / \text{hr}) * (1 \text{ ton} / 2000 \text{ lb}) = \mathbf{0.54 \text{ lb}_{\text{VOC}} / \text{hr}} \\ & (0.538 \text{ lb}_{\text{VOC}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{2.4 \text{ tons}_{\text{VOC}} / \text{yr}} \end{aligned}$$

Source No. 18-0086-25, Two Natural Gas-Fired Dryers, Uncontrolled Maximum Potential Emissions

Emissions for the following pollutants are estimated using AP-42 factors for natural gas combustion section 1.4.

Btu input = 4,000,000 Btu/hr

$$\text{Fuel Usage:} \quad (4,000,000 \text{ Btu} / \text{hr}) * (1 \text{ ft}^3 \text{ natural gas} / 1,020 \text{ Btu}) = \mathbf{3,922 \text{ ft}^3 / \text{hr}}$$

$$\begin{aligned} \text{PM:} & (7.6 \text{ lbs} / 1,000,000 \text{ ft}^3) * (3,922 \text{ ft}^3 / \text{hr}) = \mathbf{0.03 \text{ lb} / \text{hr}} \\ & (0.030 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.13 \text{ ton} / \text{yr}} \end{aligned}$$

$$\begin{aligned} \text{SO}_2: & (0.6 \text{ lb} / 1,000,000 \text{ ft}^3) * (3,922 \text{ ft}^3 / \text{hr}) = \mathbf{0.0 \text{ lb} / \text{hr}} \\ & (0.00 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.0 \text{ ton} / \text{yr}} \end{aligned}$$

$$\begin{aligned} \text{CO:} & (84 \text{ lbs} / 1,000,000 \text{ ft}^3) * (3,922 \text{ ft}^3 / \text{hr}) = \mathbf{0.33 \text{ lb} / \text{hr}} \\ & (0.329 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{1.4 \text{ tons} / \text{yr}} \end{aligned}$$

$$\text{VOC: } (5.5 \text{ lbs} / 1,000,000 \text{ ft}^3) * (3,922 \text{ ft}^3 / \text{hr}) = \mathbf{0.02 \text{ lb} / \text{hr}}$$

$$(0.022 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.09 \text{ ton} / \text{yr}}$$

$$\text{NO}_x: (100 \text{ lbs} / 1,000,000 \text{ ft}^3) * (3,922 \text{ ft}^3 / \text{hr}) = \mathbf{0.392 \text{ lb} / \text{hr}}$$

$$(0.3922 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{1.72 \text{ tons} / \text{yr}}$$

Source No. 18-0086-26, Three tile presses and two tile glazing lines with baghouse control, Uncontrolled Maximum Potential Emissions

Emissions for particulate matter are conservatively estimated based on the permitted maximum rate. This dust collection system has attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for this source are calculated post baghouse.

$$\text{PM: } \mathbf{0.5 \text{ lb}_{PM} / \text{hr}}$$

$$(0.5 \text{ lb}_{PM} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{2.2 \text{ tons}_{PM} / \text{yr}}$$

Source No. 18-0086-27, Natural Gas-Fired Tile Mounting Machine, Uncontrolled Maximum Potential Emissions

Emissions for the following pollutants are estimated using AP-42 factors for natural gas combustion section 1.4.

Btu input = 2,000,000 Btu/hr

$$\text{Fuel Usage: } (2,000,000 \text{ Btu} / \text{hr}) * (1 \text{ ft}^3 \text{ natural gas} / 1,020 \text{ Btu}) = \mathbf{1,961 \text{ ft}^3 / \text{hr}}$$

$$\text{PM: } (7.6 \text{ lbs} / 1,000,000 \text{ ft}^3) * (1,961 \text{ ft}^3 / \text{hr}) = \mathbf{0.01 \text{ lb} / \text{hr}}$$

$$(0.015 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.07 \text{ ton} / \text{yr}}$$

$$\text{SO}_2: (0.6 \text{ lb} / 1,000,000 \text{ ft}^3) * (1,961 \text{ ft}^3 / \text{hr}) = \mathbf{0.0 \text{ lb} / \text{hr}}$$

$$(0.00 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.0 \text{ ton} / \text{yr}}$$

$$\text{CO: } (84 \text{ lbs} / 1,000,000 \text{ ft}^3) * (1,961 \text{ ft}^3 / \text{hr}) = \mathbf{0.16 \text{ lb} / \text{hr}}$$

$$(0.165 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.72 \text{ tons} / \text{yr}}$$

$$\text{VOC: } (5.5 \text{ lbs} / 1,000,000 \text{ ft}^3) * (1,961 \text{ ft}^3 / \text{hr}) = \mathbf{0.01 \text{ lb} / \text{hr}}$$

$$(0.011 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{0.05 \text{ ton / yr}}$$

$$\text{NO}_x: (100 \text{ lbs / 1,000,000 ft}^3) * (1,961 \text{ ft}^3 / \text{hr}) = \mathbf{0.196 \text{ lb / hr}}$$

$$(0.1961 \text{ lb / hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{0.859 \text{ tons / yr}}$$

Source No. 18-0086-28, Four tile glazing lines with four baghouses, Uncontrolled Maximum Potential Emissions

Emissions for particulate matter are conservatively estimated based on the permitted maximum rate. This dust collection system has attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for this source are calculated post baghouse.

$$\text{PM: } \mathbf{0.46 \text{ lb}_{PM} / \text{hr}}$$

$$(0.46 \text{ lb}_{PM} / \text{hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{2.0 \text{ tons}_{PM} / \text{yr}}$$

Source No. 18-0086-29, Kiln 4 loading operation, Uncontrolled Maximum Potential Emissions

Emissions for particulate matter are conservatively estimated based on the permitted maximum rate. This dust collection system has attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for this source are calculated post baghouse.

$$\text{PM: } \mathbf{0.063 \text{ lb}_{PM} / \text{hr}}$$

$$(0.063 \text{ lb}_{PM} / \text{hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{0.276 \text{ tons}_{PM} / \text{yr}}$$

Source No. 18-0086-30, Stain milling operation, Uncontrolled Maximum Potential Emissions

Emissions for particulate matter are conservatively estimated based on the permitted maximum rate. This dust collection system has attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for this source are calculated post baghouse.

$$\text{PM: } \mathbf{0.063 \text{ lb}_{PM} / \text{hr}}$$

$$(0.063 \text{ lb}_{PM} / \text{hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{0.276 \text{ tons}_{PM} / \text{yr}}$$

Source No. 18-0086-32, Diesel-fired Emergency Generator, Uncontrolled Maximum Potential Emissions

Emissions for the following pollutants are estimated using emission factors from AP-42, section 3.3, Table 3.3-1.

Because this is an emergency generator, potential emissions will be based on an annual operating time of 500 hours, based on the memorandum from John Seitz, Director of the Office of Air Quality Planning and Standards, dated September 6, 1995.

Generator HP = 380

$$\begin{aligned}\text{PM:} \quad & (0.0022 \text{ lb / HP-hr}) * (380 \text{ HP}) = \mathbf{0.84 \text{ lb / hr}} \\ & (0.836 \text{ lb / hr}) * (500 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{0.21 \text{ ton / yr}}\end{aligned}$$

$$\begin{aligned}\text{SO}_2: \quad & (0.00205 \text{ lb / HP-hr}) * (380 \text{ HP}) = \mathbf{0.78 \text{ lb / hr}} \\ & (0.779 \text{ lb / hr}) * (500 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{0.19 \text{ ton / yr}}\end{aligned}$$

$$\begin{aligned}\text{CO:} \quad & (0.00668 \text{ lb / HP-hr}) * (380 \text{ HP}) = \mathbf{2.5 \text{ lb / hr}} \\ & (2.54 \text{ lb / hr}) * (500 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{0.63 \text{ tons / yr}}\end{aligned}$$

$$\begin{aligned}\text{TOC:} \quad & (0.00247 \text{ lb / HP-hr}) * (380 \text{ HP}) = \mathbf{0.94 \text{ lb / hr}} \\ & (0.939 \text{ lb / hr}) * (500 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{0.23 \text{ ton / yr}}\end{aligned}$$

$$\begin{aligned}\text{NO}_x: \quad & (0.031 \text{ lb / HP-hr}) * (380 \text{ HP}) = \mathbf{11.8 \text{ lb / hr}} \\ & (11.78 \text{ lb / hr}) * (500 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{2.9 \text{ tons / yr}}\end{aligned}$$

Source No. 18-0086-34, Diesel-fired Emergency Generator, Uncontrolled Maximum Potential Emissions

Emissions for the following pollutants are estimated using emission factors from AP-42, section 3.3, Table 3.3-1.

Because this is an emergency generator, potential emissions will be based on an annual operating time of 500 hours, based on the memorandum from John Seitz, Director of the Office of Air Quality Planning and Standards, dated September 6, 1995.

Generator HP = 355

$$\begin{aligned}\text{PM:} \quad & (0.0022 \text{ lb / HP-hr}) * (355 \text{ HP}) = \mathbf{0.78 \text{ lb / hr}} \\ & (0.781 \text{ lb / hr}) * (500 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{0.20 \text{ ton / yr}}\end{aligned}$$

$$\text{SO}_2: \quad (0.00205 \text{ lb / HP-hr}) * (355 \text{ HP}) = \mathbf{0.73 \text{ lb / hr}}$$

$$(0.728 \text{ lb / hr}) * (500 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{0.18 \text{ ton / yr}}$$

CO: $(0.00668 \text{ lb / HP - hr}) * (355 \text{ HP}) = \mathbf{2.4 \text{ lb / hr}}$
 $(2.37 \text{ lb / hr}) * (500 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{0.59 \text{ tons / yr}}$

TOC: $(0.00247 \text{ lb / HP - hr}) * (355 \text{ HP}) = \mathbf{0.88 \text{ lb / hr}}$
 $(0.877 \text{ lb / hr}) * (500 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{0.22 \text{ ton / yr}}$

NO_x: $(0.031 \text{ lb / HP - hr}) * (355 \text{ HP}) = \mathbf{11.0 \text{ lb / hr}}$
 $(11.01 \text{ lb / hr}) * (500 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{2.8 \text{ tons / yr}}$

Source No. Not Assigned, Mingle Silos Serviced by Baghouse F-1, Uncontrolled Maximum Potential Emissions

Emissions for particulate matter are conservatively estimated based on emissions information provided by the filter supplier. This dust collection system has attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for this source are calculated post baghouse. This source exhausts outside the facility.

PM: $(13,863 \text{ ft}^3 / \text{min}) * (0.002 \text{ gr / dscf}) * (60 \text{ min / hr}) * (1 \text{ lb / 7000 gr}) = \mathbf{0.238 \text{ lb}_{PM} / \text{hr}}$
 $(0.2377 \text{ lb}_{PM} / \text{hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{1.04 \text{ tons}_{PM} / \text{yr}}$

Source No. Not Assigned, Color Room Mezzanine Serviced by Baghouse F-2, Uncontrolled Maximum Potential Emissions

Emissions for particulate matter are conservatively estimated based on emissions information provided by the filter supplier. This dust collection system has attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for this source are calculated post baghouse. This source exhausts inside the facility. The facility is considered a 50% effective settling chamber per previous agreement with TDAPC.

PM: $(1,400 \text{ ft}^3 / \text{min}) * (0.002 \text{ gr / dscf}) * (60 \text{ min / hr}) * (1 \text{ lb / 7000 gr}) * (0.5 \text{ internal exhaust factor}) = \mathbf{0.012 \text{ lb}_{PM} / \text{hr}}$
 $(0.0120 \text{ lb}_{PM} / \text{hr}) * (8760 \text{ hrs / yr}) * (1 \text{ ton / 2000 lbs}) = \mathbf{0.053 \text{ tons}_{PM} / \text{yr}}$

Source No. Not Assigned, Housekeeping vacuum F-5, Uncontrolled Maximum Potential Emissions

Emissions for particulate matter are conservatively estimated based on emissions information provided by the filter supplier. This dust collection system has attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for this source are calculated post baghouse. This source exhausts outside the facility.

$$\begin{aligned}\text{PM: } & (1,020 \text{ ft}^3 / \text{min}) * (0.0000068 \text{ gr} / \text{dscf}) * (60 \text{ min} / \text{hr}) * (1 \text{ lb} / 7000 \text{ gr}) = \mathbf{0.00 \text{ lb}_{PM} / \text{hr}} \\ & (0.000 \text{ lb}_{PM} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.00 \text{ tons}_{PM} / \text{yr}}\end{aligned}$$

Source No. Not Assigned, Raw Materials Bay Weigh Box Service by Baghouse F-7, Uncontrolled
Maximum Potential Emissions

Emissions for particulate matter are conservatively estimated based on emissions information provided by the filter supplier. This dust collection system has attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for this source are calculated post baghouse. This source exhausts outside the facility.

$$\begin{aligned}\text{PM: } & (10,319 \text{ ft}^3 / \text{min}) * (0.003 \text{ gr} / \text{dscf}) * (60 \text{ min} / \text{hr}) * (1 \text{ lb} / 7000 \text{ gr}) = \mathbf{0.265 \text{ lb}_{PM} / \text{hr}} \\ & (0.2653 \text{ lb}_{PM} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{1.16 \text{ tons}_{PM} / \text{yr}}\end{aligned}$$

Source No. Not Assigned, Ball Mill Loading Operation Serviced by Baghouse F-8, Uncontrolled
Maximum Potential Emissions

Emissions for particulate matter are conservatively estimated based on emissions information provided by the filter supplier. This dust collection system has attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for this source are calculated post baghouse. This source exhausts outside the facility.

$$\begin{aligned}\text{PM: } & (24,540 \text{ ft}^3 / \text{min}) * (0.002 \text{ gr} / \text{dscf}) * (60 \text{ min} / \text{hr}) * (1 \text{ lb} / 7000 \text{ gr}) = \mathbf{0.421 \text{ lb}_{PM} / \text{hr}} \\ & (0.4207 \text{ lb}_{PM} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{1.84 \text{ tons}_{PM} / \text{yr}}\end{aligned}$$

Source No. Not Assigned, Engobe Mixing Serviced by Baghouse F-10, Uncontrolled Maximum Potential Emissions

Emissions for particulate matter are conservatively estimated based on emissions information provided by the filter supplier. This dust collection system has attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for this source are calculated post baghouse. This source exhausts inside the facility. The facility is considered a 50% effective settling chamber per previous agreement with TDAPC.

$$\text{PM: } (790 \text{ ft}^3 / \text{min}) * (0.01 \text{ gr} / \text{dscf}) * (60 \text{ min} / \text{hr}) * (1 \text{ lb} / 7000 \text{ gr}) * (0.5 \text{ internal exhaust factor}) =$$

0.03 lb_{PM} / hr

$$(0.034 \text{ lb}_{\text{PM}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.15 \text{ tons}_{\text{PM}} / \text{yr}}$$

Source No. Not Assigned, Press 6 Serviced by Baghouse F-11, Uncontrolled Maximum Potential Emissions

Emissions for particulate matter are conservatively estimated based on emissions information provided by the filter supplier. This dust collection system has attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for this source are calculated post baghouse. This source exhausts outside the facility.

$$\text{PM: } (15,000 \text{ ft}^3 / \text{min}) * (0.002 \text{ gr} / \text{dscf}) * (60 \text{ min} / \text{hr}) * (1 \text{ lb} / 7000 \text{ gr}) = \mathbf{0.257 \text{ lb}_{\text{PM}} / \text{hr}}$$

$$(0.2571 \text{ lb}_{\text{PM}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{1.13 \text{ tons}_{\text{PM}} / \text{yr}}$$

Source No. Not Assigned, Housekeeping Vacuum Serviced by Baghouse F-12, Uncontrolled Maximum Potential Emissions

Emissions for particulate matter are conservatively estimated based on emissions information provided by the filter supplier. This dust collection system has attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for this source are calculated post baghouse. This source exhausts inside the facility. The facility is considered a 50% effective settling chamber per previous agreement with TDAPC.

$$\text{PM: } (532 \text{ ft}^3 / \text{min}) * (0.02 \text{ gr} / \text{dscf}) * (60 \text{ min} / \text{hr}) * (1 \text{ lb} / 7000 \text{ gr}) * (0.5 \text{ internal exhaust factor}) =$$

0.05 lb_{PM} / hr

$$(0.046 \text{ lb}_{\text{PM}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.20 \text{ tons}_{\text{PM}} / \text{yr}}$$

Source No. Not Assigned, Tile Pressing Serviced by Baghouse F-17, Uncontrolled Maximum Potential Emissions

Emissions for particulate matter are conservatively estimated based on emissions information provided by the filter supplier. This dust collection system has attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for this source are calculated post baghouse. This source exhausts outside the facility.

$$\text{PM: } (50,000 \text{ ft}^3 / \text{min}) * (0.002 \text{ gr} / \text{dscf}) * (60 \text{ min} / \text{hr}) * (1 \text{ lb} / 7000 \text{ gr}) = \mathbf{0.857 \text{ lb}_{\text{PM}} / \text{hr}}$$

$$(0.8571 \text{ lb}_{\text{PM}} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{3.75 \text{ tons}_{\text{PM}} / \text{yr}}$$

Source No. Not Assigned, Equipment Cleaning Room Serviced by Baghouse F-20, Uncontrolled Maximum Potential Emissions

Emissions for particulate matter are conservatively estimated based on emissions information provided by the filter supplier. This dust collection system has attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for this source are calculated post baghouse. This source exhausts inside the facility. The facility is considered a 50% effective settling chamber per previous agreement with TDAPC.

$$\begin{aligned} \text{PM: } & (10,000 \text{ ft}^3 / \text{min}) * (0.002 \text{ gr} / \text{dscf}) * (60 \text{ min} / \text{hr}) * (1 \text{ lb} / 7000 \text{ gr}) * (0.5 \text{ internal exhaust factor}) \\ & = \mathbf{0.086 \text{ lb}_{PM} / \text{hr}} \\ & (0.086 \text{ lb}_{PM} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.375 \text{ tons}_{PM} / \text{yr}} \end{aligned}$$

Source No. Not Assigned, Maintenance Welding Shop Serviced by Baghouse, Uncontrolled Maximum Potential Emissions

Emissions for particulate matter are conservatively estimated based on emissions information provided by the filter supplier. This dust collection system has attributes that allow us to define it as inherent process equipment. Thus, potential particulate matter emissions for this source are calculated post baghouse. This source exhausts inside the facility. The facility is considered a 50% effective settling chamber per previous agreement with TDAPC.

$$\begin{aligned} \text{PM: } & (1,780 \text{ ft}^3 / \text{min}) * (0.01 \text{ gr} / \text{dscf}) * (60 \text{ min} / \text{hr}) * (1 \text{ lb} / 7000 \text{ gr}) * (0.5 \text{ internal exhaust factor}) = \\ & \mathbf{0.08 \text{ lb}_{PM} / \text{hr}} \\ & (0.076 \text{ lb}_{PM} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.33 \text{ tons}_{PM} / \text{yr}} \end{aligned}$$

Source No. Not Assigned, Natural Gas-Fired Trim Tile Dryer, Uncontrolled Maximum Potential Emissions

Emissions for the following pollutants are estimated using AP-42 factors for natural gas combustion section 1.4.

$$\text{Btu input} = 6,690,000 \text{ Btu/hr}$$

$$\text{Fuel Usage: } (6,690,000 \text{ Btu} / \text{hr}) * (1 \text{ ft}^3 \text{ natural gas} / 1,020 \text{ Btu}) = \mathbf{6,559 \text{ ft}^3 / \text{hr}}$$

$$\begin{aligned} \text{PM: } & (7.6 \text{ lbs} / 1,000,000 \text{ ft}^3) * (6,559 \text{ ft}^3 / \text{hr}) = \mathbf{0.05 \text{ lb} / \text{hr}} \\ & (0.050 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.22 \text{ ton} / \text{yr}} \end{aligned}$$

SO₂: $(0.6 \text{ lb} / 1,000,000 \text{ ft}^3) * (6,559 \text{ ft}^3 / \text{hr}) = \mathbf{0.0 \text{ lb} / \text{hr}}$
 $(0.00 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.0 \text{ ton} / \text{yr}}$

CO: $(84 \text{ lbs} / 1,000,000 \text{ ft}^3) * (6,559 \text{ ft}^3 / \text{hr}) = \mathbf{0.55 \text{ lb} / \text{hr}}$
 $(0.551 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{2.4 \text{ tons} / \text{yr}}$

VOC: $(5.5 \text{ lbs} / 1,000,000 \text{ ft}^3) * (6,559 \text{ ft}^3 / \text{hr}) = \mathbf{0.04 \text{ lb} / \text{hr}}$
 $(0.036 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{0.16 \text{ ton} / \text{yr}}$

NO_x: $(100 \text{ lbs} / 1,000,000 \text{ ft}^3) * (6,559 \text{ ft}^3 / \text{hr}) = \mathbf{0.656 \text{ lb} / \text{hr}}$
 $(0.6559 \text{ lb} / \text{hr}) * (8760 \text{ hrs} / \text{yr}) * (1 \text{ ton} / 2000 \text{ lbs}) = \mathbf{2.87 \text{ tons} / \text{yr}}$