#### Plantwide Emission Summary Hormann LLC

Sparta, TN		

				Criteria I	Poluttant Emissi	ons (tpy)			Hazardous Air Pollutant (HAP) Emissions			
Source	Description	TSP <sup>2</sup>	PM10 <sup>2</sup>	PM2.5 <sup>2</sup>	NOx	VOC	SO2	СО	CO2eq	Methylene Diphenyl Diisocyanate (MDI) CAS:101- 68-8	Styrene CAS:100-42-5	Total HAPs
001 (insignificant)	Forming Door Hardware				-	0.21						0.00
002	EPS Foam Panel Imprinting and Gluing Operation <sup>1</sup>	-			-	4.89				3.10	0.03	3.13
003	Polyurethane Foam Injection, Heat Tunnel, and Sawing Operation	2.57	2.57	2.57	0.26	25.87	0.002	0.22	318.37	0.001	-	0.001
004 (insignificant)	Custom Paint Application (Includes Paint Cure Oven Burner and Replacement Air Unit Combustion Emissions)	0.18	0.18	0.18	2.36	4.48	0.01	1.98	2,850.96			0.00
005 (insignificant)	12,000 gal Pentane (Blowing Agent) Tank Recirc Loop Components					0.58						0.00
	Totals =	2.75	2.75	2.75	2.63	36.03	0.02	2.20	3,169.33	3.10	0.03	3.13

#### Note:

1) Source 002 VOC emission calculations based on maximum garage door production of

80,000 Doors per Year

2) TSP, PM10 and PM2.5 include filterable and condensable particulate matter.

#### Hormann LLC Source 001 Forming Door Hardware

# VOC Emissions from Forming lubricant for galvanized coil forming (Insignificant Activity)

**Operating Parameters** 

Hours of Operation 8,760 hrs/yr

Lubricant Name	Annual Usage (gal)	Material Density (lb/gal)	VOC Content (%)	VOC En	nissions
Lubricant Name	Ailitual Osage (gai)	Waterial Delisity (15/gai)	VOC Content (70)	lb/year	TPY
921 DS 1MO CANT RUST (M2)	55	7.089	90%	350.9	0.18
251 ROLL FILM	10	6.672	99%	66.1	0.03
				Total	0.21

#### **Example Calculation:**

VOC Emissions = Annual Usage (gal) x Material Density (lb/gal) x VOC Content (%)

Summary

Source Summary	VOC		HAP (S	tyrene)	HAPs	<b>HAPs Total</b>	
	lb/hr	TPY	lb/hr	TPY	lb/hr	tpy	tpy
Emissions from EPS Panel	0.41	1.79	0.01	0.03			0.03
Emissions from Gluing EPS Foam	0.71	3.10			0.71	3.10	3.10
Total	1.12	4.89	0.01	0.03	0.71	3.10	3.13

#### Imprinting Panel Shape in EPS Foam<sup>1</sup>

#### **VOC Emissions from EPS Foam Loss during Imprinting Door Foam Panels.**

EPS = Expanded Polystryene

Direct Data Entry

**Operating Parameters** 

Hours of Operation 8,760 hrs/yr

Ventilation Rate 10,600 CFM (assumed) 2.12 ft 3000 fpm

Foam Loss Calculation:

24 Impressions per average 12 ft by 7

Number of impressions ft Door

Production Rate<sup>1</sup> 80,000 Doors produced per year

Foam Loss Rate (Volume) 0.0334 Ft<sup>3</sup> of foam is burned away per impression

**Annual Imprinting EPS Foam Loss** 

(Volume) 64,128 Ft<sup>3</sup> of foam burned away per year (from imprinting)

Assumed additional Foam loss from

window cutting and router

1.5% Margin of Safety - from cutting panels with hot wire or routers for windows

Annual Total Foam Loss (volume) 65,090 Ft<sup>3</sup> of foam lost annually from imprinting and cutting

**Emission Calculation:** 

EPS Foam Density 1.0 pcf or lb/ft<sup>3</sup> Nominally 1pcf per EPS Foam Tech Sheet

Tolerance for Density Variance 10%

EPS Foam VOC Content

5% per EPS Foam SDS from Pentanes
EPS Foam HAP Content

0.10% Styrene content per EPS Foam SDS

Source Summary	VC	C <sup>2</sup>	HAP (Styrene)		
	lb/hr	TPY	lb/hr	TPY	
Emissions from EPS Panel Imprinting and Cutting	0.41	1.79	0.01	0.03	

#### **Notes and Example Calculation:**

1) VOC emission calculations based on maximum garage door production of

80,000 Doors per Year

50 ft/s

2) VOC emissions (TPY) = [EPS Foam Density (pcf) x Annual EPS Foam Loss from Imprinting and cutting (ft<sup>3</sup>) x EPS Foam VOC Content(%)]/2,000 lb/ton

#### Hormann LLC Source 002 EPS Foam Panel Gluing Emissions

# **VOC and HAP Emissions from Annual Usage of PURMELT Adhesive**

#### Direct Data Entry

**Operating Parameters** 

Hours of Operation 8,760 hrs/yr

**HAP Content** 

**PURMELT 513C GLUE contains** 

Percent Methylenebis(phenylisocyanate). Also known as MDI. CAS number 101-68-8

Input Rate

Current Annual Usage of EPS Foam Panel Glue

(PURMELT 513C)

61,920 Lbs per year

7.07 lb/hr

Multiplier for increased production

2 Assumed that at full capacity for 1 shift at the TN plant, production/glue usage doubles.

Source Summary	HAPs (VOC	) from MDI	
	lb/hr	tpy	
Emissions from Gluing EPS Foam to	0.71	3.10	
Door Panels	0.71	3.10	

#### **Example Calculation:**

HAP Emissions from MDI (tpy) = [Annual usage of PURMELT 513C (lbs/yr) x Multiplier for increased production x Content (%)] / 2,000 lb/ton

HAP

Summary

Emission Point	Source Summary	Pl	М	N	Ох	V	C		SO2	C	0	CO2eq	HAPs (MDI)
		lb/hr	TPY	lb/hr	TPY	lb/hr	TPY	lb/hr	TPY	lb/hr	TPY	TPY	TPY
002.1	Polyurethane Foam Injection					5.79	25.35			1			0.001
003-1	Heat Tunnel	0.00	0.02	0.06	0.26	0.00	0.01	0.00	1.58E-03	0.05	0.22	318.37	0.000
-	Subtotal	0.00	0.02	0.06	0.26	5.79	25.36	0.00	1.58E-03	0.05	0.22	318.37	0.001
_													
003-2	Sawing	0.58	2.55							-			
003-2	Sawing VOCs		-	1	-	0.12	0.51	1	1	ı			
	Subtotal	0.58	2.55	0.00	0.00	0.12	0.51	0.00	0.00E+00	0.00	0.00	0.00	0.000
9	Source 003 Total	0.59	2.57	0.06	0.26	5.91	25.87	0.00	1.58E-03	0.05	0.22	318.37	0.001

#### Hormann LLC Source 003 Polyurethane Foam Injection VOC emissions from blowing agent, MDI

#### VOC (Pentane) Emissions

#### **Development of Emission Factor**

	Direct data entry	
Average Pentane (blowing agent) added	77.16	lb/hr
Assumed Pentane Released in Manufacturing	7.5%	Note 1
Average inlet mass to ATM	5.79	lb/hr
Emission Factor	0.075	lb VOC to ATM/lb Pentane added

#### **VOC Emissions from Manufacturing**

Maximum Annual Pentane Usage (Blowing Agent added to process)		VOC Emis	sions
(lbs/yr)	<b>Emission Factor</b>	(lbs/yr)	(TPY)
675,930	0.075	50,695	25.35

#### Notes and Example Calculation:

- 1) Conservative Estimate based upon engineering judgement and testing results in similar industry processes.
- 2) VOC Emissions (TPY) = [Maximum Pentane Added(lbs/yr) x Emission Factor(lb VOC to ATM/lb Pentane added)]/2,000 lb/ton

# Source 003 Polyurethane Foam Injection VOC emissions from blowing agent, MDI Fugitive Emissions MDI - HAPs

MDI Calculations RCAP Combined Page 104 (App A) Vapor Pressure / Temperature chart

Page 109 (App B) Vapor Pressure Adjustment Factors (K)

#### **Emission Calculation Development (MDI)**

			Per Production Data	Consumption	on at max production	
Average Foam Injection rate	3,741	lb/hr		kg/hr	lb/hr	
MDI Introduced	2,282	lb/hr	Pentane	35	77.2	
L <sub>c</sub> (MDI Emissions) =	0.9616	lb/yr	MDI	1,035	2281.8	
			Polyol	627	1382.3	
			Total	1,697	3,741.2	
Margin of Compliance <sup>1</sup> =	15%					
L. (MDI Emissions) =	1.1058	lb/vr				

#### **Equation for Calculating Stack Emissions of MDI from Doors**

#### Section 10.0 page 5-25 of MDI Emissions Reporting Guidelines for the Polyurethanes Industry

Lc = Vair \* (1 / 359) \* (273.15 / Tproc) \* (VPMDI / 760) \* Mw \* KMDI

Tproc =	158 °F (or 70°C in the polyurethane line heat tunnel)	
Tproc =	343.15 K	
VP <sub>MDI</sub> =	1.36E-03 mm Hg per App A MDI Emissions Reporting Guid	elines
Mw =	250.26 this is the molecular weight of MDI	
K <sub>MDI</sub> =	0.659 adjustment factor (function of MDI Concentration in feedstoc Reporting Guidelines	k and temperature) App B MDI Emissions
359	359 the molar volume of an ideal gas in ft <sup>3</sup> /lh-mole @ 0°C and 1-a	tmosnhere

59 359 the molar volume of an ideal gas in ft³/lb-mole @ 0°C and 1-atmosphere

Mixture = 61% MDI 61.0%

#### Vair (Annual Volume of Air Displaced)

Door Section Volume		
Avg. Section Height	21	inch
Avg. Section Thickness	1.75	inch
Avg. Section Width	12	ft

Volume per section	3.0625	ft <sup>3</sup>
Average Door Number of		sections / garage
sections	6	door
Production rate Number of		
sections/yr	480,000	sections/year

Annual Volume of Air displaced	
= Vair =	1,470,000 ft <sup>3</sup>

#### **MDI Emissions Calculations**

Max. MDI Usage	MDI Fugitive Emissions				
(lbs/yr)	(lb/yr)	(tpy)			
19,988,226	1.11	0.001			

#### Notes:

(1) Based on process knowledge, variability is estimated at 10%. A conservative value of 15% is used in calculations. This value may be adjusted in the future as additional emissions data is obtained.

#### **Operating Parameters**

Fuel Type Natural Gas

Maximum Firing Rate

Unit Description (MMBtu/hr)

Heat Tunnel for Polyurethane Foam Injection 0.614 MMBtu/hr
Operating hours 8,760 hr/yr

Annual Fuel Usage	N	atural Gas	Hou	rly Usage
Heat Tunnel	5.27	MMCF/yr	602	Cu. Ft./hr

#### **Emission Calculations**

# Emission Factors for Natural Gas Combustion 1,2

	lb/10 <sup>6</sup> scf	lb/MMBtu-HHV	
Particulate Matter ( $PM_{Total}$ )	7.6	0.0075	AP-42
Particulate Matter (PM <sub>Cond</sub> )	5.7	0.0056	AP-42
Particulate Matter $(PM_{Filter})^3$	1.9	0.0019	AP-42
Nitrogen Oxides (NO <sub>x</sub> )	100	0.0980	AP-42
Carbon Monoxide (CO)	84	0.0820	AP-42
Sulfur Dioxide (SO <sub>2</sub> )	0.6	0.0006	AP-42
VOC	5.5	0.0054	AP-42
Carbon Dioxide (CO <sub>2</sub> )	120,000	117.65	AP-42
Methane (CH <sub>4</sub> )	2.3	2.255E-03	AP-42
Nitrous Oxide (N <sub>2</sub> O)	2.2	2.157E-03	AP-42

#### **Natural Gas Emissions**

#### Heat Tunnel

		Annual <sup>4,5</sup>
	lb/hr	ton/year
Particulate Matter (PM <sub>Total</sub> ) <sup>3</sup>	0.00	0.02
Particulate Matter (PM <sub>10</sub> ) <sup>3</sup>	0.00	0.02
Particulate Matter (PM <sub>2.5</sub> ) <sup>3</sup>	0.00	0.02
Nitrogen Oxides (NO <sub>x</sub> )	0.06	0.26
Carbon Monoxide (CO)	0.05	0.22
Sulfur Dioxide (SO <sub>2</sub> )	0.000	1.58E-03
Combustion VOC	0.00	0.01
Carbon Dioxide (CO <sub>2</sub> )	72	316
Methane (CH <sub>4</sub> )	0.00	0.01
Nitrous Oxide (N <sub>2</sub> O)	1.32E-03	0.006
CO <sub>2</sub> Equivalent (CO <sub>2</sub> eq) <sup>7</sup>		318

GWP <sup>6</sup>					
CH4	25				
N2O	298				

#### **Example Calculations/Notes:**

- (1) Compilation of Air Pollutant Emission Factors, AP-42, Supplement D, Fifth Edition, Section 1.4, Tables 1.4-1 and 1.4-2, July 1998, Small Boilers < 100 MMBtu/hr
- (2) Per AP-42, Table 1.4-1 and 1.4-2, to convert from  $lb/10^6$  scf to  $kg/10^6$  m<sup>3</sup>, multiply by 16. To convert from  $lb/10^6$  scf to lb/MMBtu, divide by 1,020.
- (3) Assume  $PM_{Total} = PM_{2.5} = PM_{10}$ . (Includes filterable and condensable particulate matter)
- (4) Maximum Emissions (lb/hr) = Emission Factor (lb/MMscf) \* Natural Gas Usage (MMCF)
- (5) Annual Emissions (tpy) = Average Emissions (lb/hr) \* 8,760 (hr/yr) / 2,000 (lb/ton)
- (6) GWP from 40 CFR 98 Subpart A Table A-1
- (7)  $CO_2$  Equivalent ( $CO_2$ eq) =  $CO_2$  + [ $GWP_{CH4}$  \*  $CH_4$ ] + [ $GWP_{N2O}$  \*  $N_2O$ ]

#### Polyurethane Foam Injection Line Sawing Operation: VOC released to Dust Collector

Operating Parameters

Hours of Operation

8,760 hrs/yr

#### Maximum Potential to Emit - VOC

Maximum Annual Pentane Usage	VOC Loss at Manufacturing	VOC Available at Sawing <sup>1</sup>	Section Foam Trimmed <sup>2,3</sup>	VOC Emi	issions <sup>4,5</sup>
(lbs/yr)	(lbs/yr)	(lbs/yr)	(%)	(lbs/yr)	(tpy)
675,930	50,695	625,236	0.16%	1,026	0.51

lb/hr 0.12

#### Notes:

- (1) VOC Available at Sawing (lbs) = Max Blowing Agent VOC (lbs) VOC Loss at Manufacturing (lbs)
- (2) The maximum cut volume is determined first by calculating the trim from each side of the garage door section. As indicated, automated saws trim the edges of the doors, trimming approximately 3mm from each side. Average Garage door section width is 12 ft, average section height is 21 inch, and the average section thickness is 1.75 inch. All saw cut emissions are collected and routed to the baghouse dust collector. The table below contains a detailed calculation of the % volume cut during sawing.
- (3) Assume that the mass of trimmed door section is proportional to volume (0.16%).
- (4) VOC Emissions (lbs) = VOC Available at Sawing (lbs) \* Section Foam Trimmed (%) / 100
- (5) VOC Emissions (tons) = VOC Emissions (lbs) / 2000

Volume	0.16%	
Percentage of Total		
section	2	cuts
Number of cuts per		
Volume Trimmed/cut	0.0025	ft <sup>3</sup>
Saw Kerf	3	mm
Volume of Section Trimmed		
Section	3.00	it.
Volume of Untrimmed Section	3.06	ft <sup>3</sup>
Avg. Section Width	12	ft
Avg. Section Thickness		inch
Avg. Section Height		inch
Door Section Volume		

#### **Sawing Dust Collector Emissions**

Operating Hours 8,760 hr/yr

Baghouse I.D.	Flow Rate (ACFM)	Exhaust Diameter (ft)	Exhaust Cross-Sectional Area (ft²)	Exit Velocity (ft/sec)	Exit Velocity (ft/min)	Exit Temp (F)	Moisture Content %	Flow Rate <sup>1</sup> (DSCFM)	Exhaust PM Conc. (gr/dscf)	PI lb/hr²	tpy <sup>3</sup>
Sawing DC	3,531	1.22	1.18	50.0	3000.0	80	2.0%	3,397	0.02	0.58	2.55

#### Example Calculations and Notes:

- (1) Flow Rate (DSCFM) = (ACFM x ((460+70)/(460 + Exit Temp))) x (1 Moisture Content)
- (2) PM Emissions (lb/hr) = DSCFM x Exhaust PM Conc. x 60 (min/hr) x (1 lb / 7000 grains)
- (3) PM Emissions (tpy) = (PM Emissions (lb/hr) x 8760 (hr/yr)) / (2000 (lb/ton))

Summary

<b>Emission Point</b>	Source Summary	P	М	N	Ох	V	oc	S	02	С	0	CO2eq	HAPs (MDI)
		lb/hr	TPY	lb/hr	TPY	lb/hr	TPY	lb/hr	TPY	lb/hr	TPY	TPY	TPY
004-1	Custom Paint Application	2.54	3.05			3.63	4.35						0.001
004-2	Replacement Air	0.02	0.10	0.29	1.29	0.02	0.07	0.00	0.01	0.25	1.08	1555.07	
004-3	Custom Paint Cure Oven	0.02	0.08	0.25	1.07	0.01	0.06	0.00	0.01	0.21	0.90	1295.89	
	Subtotal	2.59	3.23	0.54	2.36	3.65	4.48	0.00	0.014	0.45	1.98	2850.96	0.001

# Hormann LLC Source 004 Custom Paint Application VOC Emissions from Annual Usage of Custom Paint

**Operating Parameters** 

Hours of Operation 8,760 hrs/yr

Potential Overspray 30%

Material Density 11.7 lb/Gal
Solid Content 58% by weight

Carbithane 11 Series Low VOC Coatings 2.9 lb VOC/gal per Product Data Sheet

Custom Paint Application Annual Usage 3,000 Gallons per year

Anticipated Actual Operation 2,400 hours/yr

Source Summary	Р	М	VOC		
	lb/hr <sup>2</sup>	TPY <sup>1</sup>	lb/hr <sup>2</sup>	TPY <sup>1</sup>	
Emissions from Custom Paint Application	2.54	3.05	3.63	4.35	

#### **Example Calculation:**

- 1. PM emissions (tpy) = Coating Annual Usage (gal/yr) x Material Density (lb/gal) x Solids Content (%) x Potential Overspray (%) / 2000 lb/ton
- 2. VOC emissions (tpy) = Coating VOC Content (lb/gal) x Coating Annual Usage (gal/yr) / 2,000 lb/ton
- 3. The Lb/hr emission rate is estimated based upon this source operating at just 2,400 hrs/year due to the anticipated actual operation. Though Hormann LLC does not wish to limit the operating hours for the source.

# **Operating Parameters**

Fuel Type Natural Gas

Maximum
Firing Rate
Unit Description (MMBtu/hr)

Replacement Make-up Air Unit 3.00 MMBtu/hr
Operating hours 8,760 hr/yr

Annual Fuel Usage Natural Gas Hourly Usage
Replacement Make-up Air Unit 25.76 MMCF/yr 2,941 Cu. Ft./hr

### **Emission Calculations**

# **Emission Factors for Natural Gas Combustion** 1,2

	<u>lb/10<sup>6</sup> scf</u>	Ib/MMBtu-HHV	
Particulate Matter (PM <sub>Total</sub> )	7.6	0.0075	AP-42
Particulate Matter (PM <sub>Cond</sub> )	5.7	0.0056	AP-42
Particulate Matter (PM <sub>Filter</sub> ) <sup>3</sup>	1.9	0.0019	AP-42
Nitrogen Oxides (NO <sub>x</sub> )	100	0.0980	AP-42
Carbon Monoxide (CO)	84	0.0820	AP-42
Sulfur Dioxide (SO <sub>2</sub> )	0.6	0.0006	AP-42
VOC	5.5	0.0054	AP-42
Carbon Dioxide (CO <sub>2</sub> )	120,000	117.65	AP-42
Methane (CH <sub>4</sub> )	2.3	2.255E-03	AP-42
Nitrous Oxide (N <sub>2</sub> O)	2.2	2.157E-03	AP-42

# **Natural Gas Emissions**

# **Replacement Air Make-up Unit**

•		Annual <sup>4,5</sup>
	lb/hr	ton/year
Particulate Matter (PM <sub>Total</sub> ) <sup>3</sup>	0.02	0.10
Particulate Matter (PM <sub>10</sub> ) <sup>3</sup>	0.02	0.10
Particulate Matter (PM <sub>2.5</sub> ) <sup>3</sup>	0.02	0.10
Nitrogen Oxides (NO <sub>x</sub> )	0.29	1.29
Carbon Monoxide (CO)	0.25	1.08
Sulfur Dioxide (SO <sub>2</sub> )	0.002	0.01
Combustion VOC	0.02	0.07
Carbon Dioxide (CO <sub>2</sub> )	353	1,546
Methane (CH <sub>4</sub> )	0.01	0.03
Nitrous Oxide (N <sub>2</sub> O)	6.47E-03	0.028
CO <sub>2</sub> Equivalent (CO <sub>2</sub> eq) <sup>7</sup>		1,555

GWP <sup>6</sup>		
CH4	25	
N2O	298	

# **Example Calculations/Notes:**

- (1) Compilation of Air Pollutant Emission Factors, AP-42, Supplement D, Fifth Edition, Section 1.4, Tables 1.4-1 and 1.4-2, July 1998, Small Boilers < 100 MMBtu/hr
- (2) Per AP-42, Table 1.4-1 and 1.4-2, to convert from  $lb/10^6$  scf to  $kg/10^6$  m<sup>3</sup>, multiply by 16. To convert from  $lb/10^6$  scf to lb/MMBtu, divide by 1,020.
- (3) Assume  $PM_{Total} = PM_{2.5} = PM_{10}$ . (Includes filterable and condensable particulate matter)
- (4) Maximum Emissions (lb/hr) = Emission Factor (lb/MMscf) \* Natural Gas Usage (MMCF)
- (5) Annual Emissions (tpy) = Average Emissions (lb/hr) \* 8,760 (hr/yr) / 2,000 (lb/ton)
- (6) GWP from 40 CFR 98 Subpart A Table A-1
- (7)  $CO_2$  Equivalent ( $CO_2$ eq) =  $CO_2$  + [ $GWP_{CH4}$  \*  $CH_4$ ] + [ $GWP_{N2O}$  \*  $N_2O$ ]

004-3

# **Operating Parameters**

Fuel Type Natural Gas

Maximum Firing Rate

Unit Description (MMBtu/hr)

Custom Paint Cure Oven Burner 2.50 MMBtu/hr
Operating hours 8,760 hr/yr

Annual Fuel Usage	Natural Gas		Hourly Usage			
Custom Paint Cure Oven Burner	21.47	MMCF/yr		2,451	Cu. Ft./hr	

# **Emission Calculations**

# **Emission Factors for Natural Gas Combustion** 1,2

	lb/10 <sup>6</sup> scf	lb/MMBtu-HHV	
Particulate Matter (PM <sub>Total</sub> )	7.6	0.0075	AP-42
Particulate Matter (PM <sub>Cond</sub> )	5.7	0.0056	AP-42
Particulate Matter (PM <sub>Filter</sub> ) <sup>3</sup>	1.9	0.0019	AP-42
Nitrogen Oxides (NO <sub>x</sub> )	100	0.0980	AP-42
Carbon Monoxide (CO)	84	0.0820	AP-42
Sulfur Dioxide (SO <sub>2</sub> )	0.6	0.0006	AP-42
VOC	5.5	0.0054	AP-42
Carbon Dioxide (CO <sub>2</sub> )	120,000	117.65	AP-42
Methane (CH <sub>4</sub> )	2.3	2.255E-03	AP-42
Nitrous Oxide (N <sub>2</sub> O)	2.2	2.157E-03	AP-42

# **Natural Gas Emissions**

# **Custom Paint Cure Oven**

	lb/hr	Annual <sup>4,5</sup> ton/year
Particulate Matter (PM <sub>Total</sub> ) <sup>3</sup>	0.02	0.08
Particulate Matter (PM <sub>10</sub> ) <sup>3</sup>	0.02	0.08
Particulate Matter $(PM_{2.5})^3$	0.02	0.08
Nitrogen Oxides (NO <sub>x</sub> )	0.25	1.07
Carbon Monoxide (CO)	0.21	0.90
Sulfur Dioxide (SO <sub>2</sub> )	0.001	0.01
Combustion VOC	0.01	0.06
Carbon Dioxide (CO <sub>2</sub> )	294	1,288
Methane (CH <sub>4</sub> )	0.01	0.02
Nitrous Oxide (N <sub>2</sub> O)	5.39E-03	0.024
CO <sub>2</sub> Equivalent (CO <sub>2</sub> eq) <sup>7</sup>		1,296

GWP <sup>6</sup>		
CH4	25	
N2O	298	

# **Example Calculations/Notes:**

- (1) Compilation of Air Pollutant Emission Factors, AP-42, Supplement D, Fifth Edition, Section 1.4, Tables 1.4-1 and 1.4-2, July 1998, Small Boilers < 100 MMBtu/hr
- (2) Per AP-42, Table 1.4-1 and 1.4-2, to convert from  $lb/10^6$  scf to  $kg/10^6$  m<sup>3</sup>, multiply by 16. To convert from  $lb/10^6$  scf to lb/MMBtu, divide by 1,020.
- (3) Assume  $PM_{Total} = PM_{2.5} = PM_{10}$ . (Includes filterable and condensable particulate matter)
- (4) Maximum Emissions (lb/hr) = Emission Factor (lb/MMscf) \* Natural Gas Usage (MMCF)
- (5) Annual Emissions (tpy) = Average Emissions (lb/hr) \* 8,760 (hr/yr) / 2,000 (lb/ton)
- (6) GWP from 40 CFR 98 Subpart A Table A-1
- (7)  $CO_2$  Equivalent ( $CO_2$ eq) =  $CO_2$  + [ $GWP_{CH4}$  \*  $CH_4$ ] + [ $GWP_{N2O}$  \*  $N_2O$ ]

13. Outage: Average distance	e in feet from top	Average throughput	Maximum number of tank				
of tank to liquid surface.		(gallons/day)	turnovers per year				
14. Complete the following only if the tank is equipped with a floating roof:							
A. Roof type:	Doub <u>le</u> deck	Pontoon Pan	Other (describe)				
B. Seal type:	Single	Double	Other (describe)				
C. Shell construction:	Riveted	Welded	Other (describe)				
15. Comments							
	1000	SIGNATURE					
			n a signature is not required on this form.				
Date this form regardless of w time as an APC 100 form, then		· ·	n is NOT being submitted at the same				
			as the responsible person of the above				
			on is accurate and true to the best of my smade under penalty of perjury.				
16. Signature			Date ,				
			17 Sept. 2018				
Signer's name (type or pr	int) Titl	e 11 11= 110	Phone number with area code				
Camton Kudd	Me.	sident, Hormann UC	630-518-0623				

#### **Hormann LLC**

#### **Blowing Agent Component Fugitive Emissions**

#### Source 005

The tank has a nitrogen blanket. Therefore, no emissions are calculated from the tank itself.

**Operating Parameters** 

Hours of Operation 8,760 hrs/yr

The blowing agent tank has a recirculating pump and loop that runs continually. The process draws blowing agent off this loop as required for production. The loop fittings are included. Fugitive blowing agent emissions from leaks in the transfer lines and the process piping were calculated using US EPAs publication

lb/hr/component

"Fugitive VOC Emissions in the Synthetic Organic Chemical Manufacturing Industry (SOCMI)", December 1984 (EPA-625/10-84-004) Emission Factors

The factors presented in the original publication were revised based on June 1994 guidance from the Texas Natural Resource Conservation Commission (TNRCC).

The most conservative factors (i.e. light liquids) were used to represent blowing agent. The emission factors are as follows:

Valves	0.0035	lb/hr/component	
Pump Seals	0.0386	lb/hr/component	
Flanges	0.0005	lb/hr/component	
Relief Valves**	0.22963	lb/hr/component	

Hormann expects that the blowing agent transfer and process system will consist of a maximum of 2 pumps, 27 flanged connections, 12 valves, and 2 relief valves.

Therefore, the minimum expected emissions from blowing agent transfer lines and process piping are:

	# of Components	% VOC in Blowing Emission Factor		VOC Emissions <sup>1,2</sup>		
Components	# or components	Agent	(lb/hr/component)	(lb/hr)	(lb/yr)	(tpy)
Valves	12		0.0035	0.04	368	0.18
Pump Seals	2	100%	0.0386	80.0	676	0.34
Flanges	27		0.0005	0.01	118.3	0.06
Relief Valves	5		0	0.00	0.0	0.00
			Total =	0.13	1,162	0.58

#### Notes:

(1) VOC Emissions (lbs) = # of Components \* % VOC in Blowing Agent (%) \* Emission Factor (lb/hr/component) / 100

(2) VOC Emissions (tpy) = VOC Emissions (lb/yr) / 2000 (lb/ton)

<sup>\*\*</sup>Because each tank will operate under pressure, there are assumed to be no emissions from pressure relief valves.